

Extracortical plate fixation with new plate inserts and cerclage wires for the treatment of periprosthetic hip fractures

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Abstract

Purpose Fixation of periprosthetic hip fractures with intracortical anchorage might not be feasible in cases with bulky implants and/or poor bone stock.

Methods Rotational stability of new plate inserts with extracortical anchorage for cerclage fixation was measured and compared to the stability found using a standard technique in a biomechanical setup using a torsion testing machine. In a synthetic PUR bone model, transverse fractures were fixed distally using screws and proximally by wire cerclages attached to the plates using “new” (extracortical anchorage) or “standard” (intracortical anchorage) plate inserts. Time to fracture consolidation and complications were assessed in a consecutive series of 18 patients (18 female; mean age 81 years, range 55–92) with periprosthetic hip fractures (ten type B1, eight type C-Vancouver) treated with the new device between July 2003 and July 2010.

Results The “new” device showed a higher rotational stability than the “standard” technique ($p < 0.001$). Fractures showed radiographic consolidation after 14 ± 5 weeks (mean \pm SD) postoperatively in patients. Revision surgery was necessary in four patients, unrelated to the new technique.

Conclusion In periprosthetic hip fractures in which fixation with intracortical anchorage using conventional means might be difficult due to bulky revision stems and/or poor bone stock, the new device may be an addition to the range of existing implants.

Keywords Periprosthetic fracture · Fixation · Extracortical · Revision stem · Elderly · Hip · Plate insert · Cerclage

Introduction

Femoral shaft fractures following total hip arthroplasty are classified using the Vancouver classification system [1]. In general, fractures with a well-fixed stem occurring around (type B) or below (type C) the femoral stem are treated by open reduction and internal fixation using plates with proximal monocortical screws, proximal cables, and distal bicortical screws [2–5]. In cases of periprosthetic fractures with osteoporotic bone combined with a thin cortex and/or bulky revision stems in situ, placement of screws might not be feasible (Fig. 1). In locking compression plates—especially when introduced for fracture fixation in the elderly with osteoporotic bone—screw placement is still a concern as the direction of the screws is predetermined by the thread in the plate for the head-locking screws. As a result, placement with abutment of the prosthesis stem leading to altered screw threads with subsequent screw pullout or fatigue failure of the plate have been described [6–8]. Moreover, proximal screws may violate the bone–prosthesis interface, lead to formation of cement cracks with subsequent prosthetic loosening, act as stress enhancers with an increasing risk for further fractures, and cerclage fixation has shown high failure rates with minimal rotational stability [9–12]. For these reasons plates for extracortical fixation using the clamp-on principle have been developed. Whereas the Mennen plate showed insufficient neutralisation of the bending moment in a relatively small series [13], the shape-memory sawtooth-arm embracing fixator was successful in stabilising Vancouver type B1 and C fractures [14]. But their utility for comminuted fractures is limited. Both types of plates involve unavoidably extensive interference with soft tissue which is of concern and

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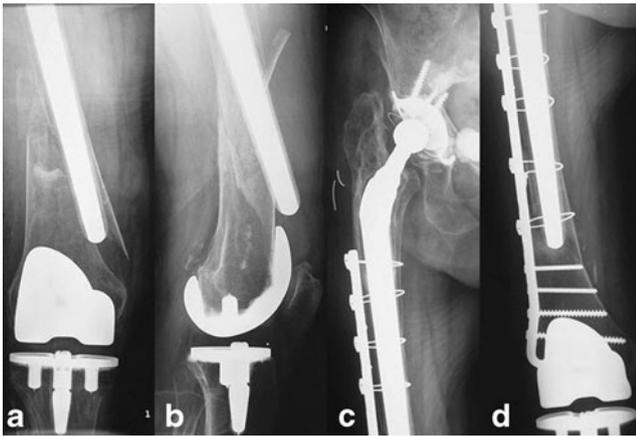


Fig. 1 Conventional radiographs AP view (a) and lateral views (b) showing a periprosthetic femoral shaft fracture in an 85-year-old female patient with thin cortical bone due to osteoporosis and a bulky revision stem in the femoral shaft. Conventional radiographs AP views (c, d) after wire-cerclage plating of a periprosthetic femoral shaft fracture using the new plate inserts

neither plates allow additional screw fixation through the plate.

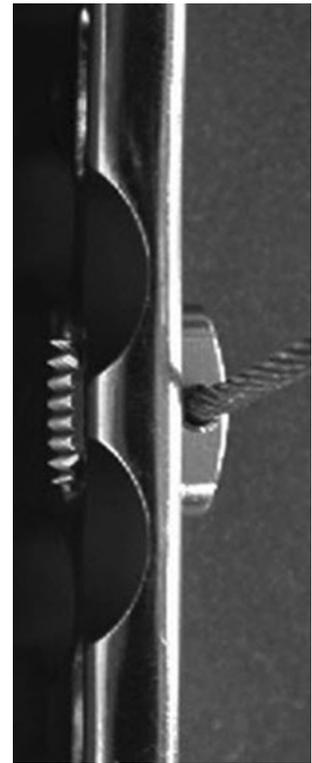
Considering all these limitations, “cerclage only” fixation of the proximal fragment might be favourable. However, the conventional cerclage positioning devices either have no bone contact or require pins through monocortical drill holes at the risk of further weakening the thin bone. Moreover, sufficient depth of the drill holes for adequate fixation seems unobtainable in the presence of a canal filling implant. As a result, they do not biomechanically operate as a screw as they hold the cerclage with minimal impact on the bone and rotational stability cannot be guaranteed. To potentially resolve these limitations, new plate inserts without the need for any drill holes have been developed with a ridged surface protruding from the plate on the bony side to hook into the bone and to provide rotational stability as an extracortical device (Fig. 2). We postulate, that the new device in combination with cerclage wire fixation provides rotational stability comparable to a cerclage fixation using the conventional positioning pins. The aim of this report was to test the hypothesis in a simplified biomechanical setup and to report preliminary results on the clinical implementation of the new device.

Methods

Biomechanical testing

A synthetic polyurethane (PUR) bone model (PR0014, Synbone, Switzerland) was used. The cylinder, with an outer diameter of 40 mm and length of 200 mm, consisted of a cortical wall thickness of three millimetres dense PUR and an

Fig. 2 Photograph showing the new insert with a ridged surface protruding from the plate on the bony side with the potential to hook into the bone and to ensure rotational stability



inner porous part simulating trabecular bone. A fracture was simulated by performing transverse osteotomies at half of the length of the cylinders. A reinforcement of the model was established by insertion of a distal part of an uncemented revision hip stem (Revitan® stem, distal straight, Zimmer, Switzerland). Reaming of the model was performed prior to insertion of the stem using a conical reamer with a diameter of 16 mm up to a depth of 60 mm. The hip stem was inserted so that the distal tip of the stem was 20 mm distal to the fracture line. The fractures were then fixed using seven-hole plates (DCP® 4.5 mm broad, stainless steel, Synthes, Zuchwil, Switzerland) with a monocortical and two bicortical screws (4.5 mm cortex screws; Synthes) in the distal three holes. Proximally, the first three holes were instrumented with a wire cerclage (diameter: 1.5 mm; Synthes) using the conventional positioning pins (Ref. 298.839; Synthes) in the control group (Fig. 3a) whereas the new inserts (custom-made device; Synthes) were used in the treatment group (Fig. 3b). To ensure comparable pre-tension and symmetrical twisting of the cerclage wires, a standardised wire tightening technique was used for all tests as published previously [15]. Thereafter, each of the reconstructions was distorted 20 times $\pm 2^\circ$ with $15^\circ/\text{s}$. After this dynamic loading a quasistatic deformation of up to a maximal angle of 5° was performed while recording the torsional moment (Nm) in both groups. Rotational stability was measured using a torsion testing machine (TL500; Zwick; for example, see Fig. 4).

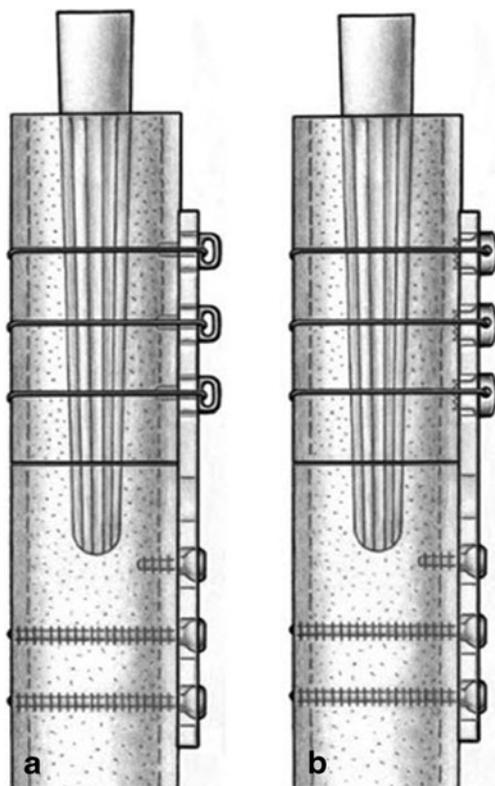


Fig. 3 Drawing of the test setup in the experimental group with the standard inserts (intracortical anchorage) (**a**) for wire cerclage fixation proximally or the new inserts (extracortical anchorage) (**b**) in a transverse fracture model in synthetic PUR bone with a revision hip stem in situ. The fracture was fixed using screws distally

Patient evaluation

Between July 2003 and July 2010, a consecutive series of 18 patients (18 female; mean age 81 years, range 55–92) with periprosthetic hip fractures at/around or distal to the prosthesis tip with a well-fixed stem were treated by the senior author using “cerclage only” fixation, supported by the new plate inserts in the proximal fragment and with bicortical screws in the distal fragment. The patients’ charts were assessed for the patients’ demographics, body mass index (kg/m^2), amount of medical comorbidities, the American Society of Anaesthesiologists Physical Status Classification (ASA) level, the time interval from the index procedure with total hip replacement up until the episode of trauma leading to periprosthetic hip fracture, the postoperative aftercare protocol, the patients’ mobility prior to trauma and after fracture healing at the latest follow-up, intra- and postoperative complications, duration of surgery and blood loss. The radiographic data was analysed to describe the fracture types according to the Vancouver classification [2] and the time until fracture union occurred. The retrospective evaluation focused on the evaluation of the time interval until the fractures were radiographically

Fig. 4 Photograph of the test setup in the group with the new device in the transverse fracture model in synthetic PUR bone with a revision hip stem in situ. The fracture was fixed using screws distally and the new plate inserts for wire cerclage fixation proximally



consolidated, full weight-bearing was allowed and any postoperative complications needing revision surgery.

Statistical analysis

In the biomechanical setup, the three replicated series “torsional load per displacement” of each group were averaged, and the averaged series analysed. Mixed-effects models with the torsional moment (Nm) as the dependent variable and polynomial trends in the rotational displacement (in degree) as a predictor were used to estimate the average curves for the treatment group “new” and for the control group “standard”. The differences in parameters of the two curves were analysed using *z*-tests. Bonferroni adjustment was applied to have an overall significance level of 5 % for all comparisons. In the clinical setup, *p*-values are not provided as the statistical analysis used was descriptive. Statistical analysis was performed with SAS 9.2 (SAS Institute Inc., Cary, NC, USA).

Results

Biomechanical testing

The averaged curves for the treatment group “new” and for the control group “standard” presenting the results for the mixed-

effects model with the torsional moment (Nm) as the dependent variable and polynomial trends of grade two in the rotational displacement (in degree) as a predictor are displayed in Fig. 5. The value (mean \pm standard error) for the slope of the curves was 1.49 ± 0.04 in the group “new” and 1.24 ± 0.04 in the group “standard”. The observed differences were statistically significant ($p < 0.001$), so that an increased torsional load was required to achieve the same rotational displacement in the treatment group using the new device compared to the control group using the standard positioning pins.

Patients

Fixation of the periprosthetic fracture was undertaken using either conventional plates in 15 of 18 cases (LC-DCP® 4.5, broad, stainless steel, Ref. 226.600; Synthes) or 95° condylar plates in three of 18 cases. In the proximal fragment, wire cerclage using the new inserts was applied, whereas in the distal fragment bicortical screws were feasible (e.g. Fig. 1c, d). Patient demographics, number of comorbidities, Vancouver classification of the fractures, time from the index procedure with total hip replacement until trauma, postoperative aftercare (partial weight bearing [PWB] = 15–20 kg), time until union, mobility before trauma and osteosynthesis, postoperative mobility after fracture consolidation, complications in the postoperative course are listed in detail in Table 1. In addition, the median body mass index (in kg/m²) was 24.8 (range 18.4–44.5) and the median ASA level was 3 (range 2–4). The time needed for surgery (mean \pm SD) was 149 ± 27 min and the estimated blood loss (mean \pm SD) was 580 ± 280 ml. Revision surgery was necessary in four of the 18 patients. In one patient, early surgical evacuation of an haematoma one day after

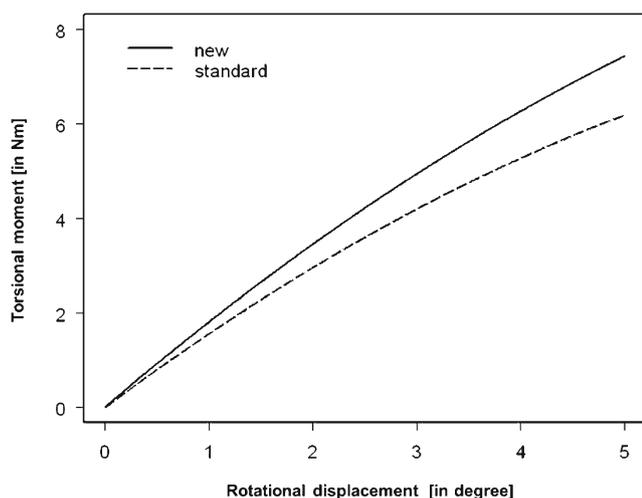


Fig. 5 Graph presenting the torsional loads per displacement (mean \pm SD; in Nm) measured for the groups using the new device (“new”) or the standard positioning pins (“standard”). Differences in the torsional moments required for rotational displacement were statistically significant ($p < 0.001$)

osteosynthesis was necessary due to anticoagulant bleeding. In two patients, revision surgery was necessary due to a re-fracture caused by repeated falls 12 or 97 days after osteosynthesis. Aseptic loosening of the prosthesis stem occurred in another patient 18 months after fixation of the periprosthetic hip fracture using the new inserts. The need for revision surgery was unrelated to the new plate insert device.

Discussion

The prevalence of periprosthetic femoral fractures ranges from 1 % in primary total hip arthroplasty to 4 % in revision total hip replacements [16]. However, due to the increasing numbers of total hip arthroplasties in combination with increasing age and growing daily activities of the elderly at risk for falls, the orthopaedic surgeon will be confronted with an increasing number of periprosthetic fractures in the elderly in the future [16, 17]. In general, treatment of these fractures is challenging as experience in the field of orthopaedic revision surgery as well as in trauma surgery is needed [18]. In particular, fixation of fractures occurring at or near the distal tip of the prosthesis with a stable femoral stem (Vancouver B1 or C) [2] is difficult as these fracture types are most frequently associated with complications, due to the inherently unstable fracture pattern [1, 19]. In cases with a poor bone stock and especially those with thin cortical bone and/or with bulky implants in situ, conventional devices may not be ideal for the stable fixation of the proximal fragment. Thus, current concepts for fracture fixation have to be reconsidered. The purpose of this study was to assess the rotational stability provided by a new fixation reconstruction using specific plate inserts with extracortical anchorage compared to a standard technique.

The stability of cerclage fixation devices depends on the “bone-to-plate” interface and the “wire-to-plate” connection. We therefore indicate that the inserts of the new device hook into the bone and have an extracortical impact on the bone without the disadvantages of conventional inserts requiring monocortical drill holes for anchorage. The “bone-to-plate” interface of these new inserts showed a footprint of the toothed surface in one patient on the occasion of a re-operation due to aseptic loosening of the stem more than one year after the index procedure. Additionally, the inserts have an oval shape ensuring stability on the part of the hardware as the rotation of the oval inserts in oval plate holes is not possible. The conventional plate inserts do not provide such a stable “wire-to-plate” connection.

Differences in torsional loads per displacement using cerclage fixation with the new inserts were statistically significant compared to conventional inserts in the biomechanical testing. In addition, in the presence of a bulky implant the necessary insertion depth of the pin may not be achievable, making the implant less stable than in the model setting. In the clinical evaluation, the use of the new device in these specific

Table 1 Patient demographics

Patient number	Age/sex	Comorbidities	Fracture	THR before	Rehabilitation protocol	Union	Pre-OP mobility	Post-OP mobility after fracture consolidation	Complications
1	92/F	1	B1	2 years	PWB—8 weeks	20 weeks	Unaided	Walking frame	Re-Fracture
2	92/F	2	C	8 years	Bed to chair—8 weeks	23 weeks	Walking frame	Walking frame	–
3	55/F	>3	B1	13 years	Bed to chair—8 weeks	20 weeks	Single stick	Single stick	Aseptic loosening
4	84/F	0	B1	17 years	PWB—8 weeks	8 weeks	Unaided	Two crutches	–
5	85/M	>3	C	6 months	Bed to chair—8 weeks	18 weeks	Unaided	Transfer to wheelchair	–
6	89/F	1	B1	17 years	Bed to chair—8 weeks	20 weeks	Unaided	Unaided	–
7	76/F	0	C	12 years	Bed to chair—8 weeks	13 weeks	Unaided	Walking frame	–
8	73/F	2	C	2 years	PWB—8 weeks	25 weeks	Unaided	Unaided	–
9	77/F	0	B1	1 year	PWB—8 weeks	12 weeks	Unaided	Single stick	–
10	84/F	2	B1	12 years	Bed to chair—8 weeks	13 weeks	Single stick	Single stick	–
11	87/F	>3	C	2 years	Bed to chair—8 weeks	13 weeks	Walking frame	Walking frame	–
12	89/F	>3	C	17 years	Bed to chair—8 weeks	15 weeks	Walking frame	Transfer to wheelchair	–
13	85/F	>3	C	4 months	PWB—8 weeks	13 weeks	Single stick	Two crutches	Re-fracture
14	74/F	>3	B1	19 years	Bed to chair—8 weeks	10 weeks	Single stick	Walking frame	–
15	86/F	3	B1	8 years	Bed to chair—8 weeks	11 weeks	Walking frame	Walking frame	–
16	70/F	0	B1	8 years	Bed to chair—8 weeks	7 weeks	Unaided	Walking frame	–
17	72/F	>3	C	3 years	Bed to chair—8 weeks	12 weeks	Unaided	Two crutches	Haematoma
18	83/F	>3	B1	2 years	Bed to chair—8 weeks	6 weeks	Two crutches	Walking frame	–

F female, M male, THR total hip replacement, PWB partial weight bearing

periprosthetic fracture patterns obtained promising results since fractures healed in all patients. However, it is questionable whether these differences—obtained in a simplified biomechanical setup—are of clinical relevance. They may even achieve less stability in the clinical situation since the thin cortical bone does not provide the same stability as the material in the model. The use of human femoral specimens, in contrast, would also be limited by the inherent variability of the specimen, requiring large sample sizes in order to obtain statistically significant results. In addition, the availability of such specimens is limited. Further limitations of the study are that (1) the relationship between the length of the plate and the length of the synthetic bone was not evaluated (a shorter fixation could prove to be less rigid), (2) isometric loading with pure torsional force application rather than physiological loading reflecting the in vivo conditions was applied and (3) the impact of soft-tissues (e.g. muscles forces) was not assessed. However, due to the reduced complexity of the model, the statistically significant differences found in fixation strength of the devices used might be related to the stiffness of the reconstruction device rather than to other influences. Additionally, the tension of the wire cerclage was not measured, so that it remains unclear whether the stiffness in terms of tension of the wires is comparable. Despite this, a standardised wire tightening technique has been used [15]. A further limitation might be that only a transverse osteotomy was used. A transverse osteotomy does, however, simulate the worst case scenario due to the high rotational instability fracture pattern.

The clinical use of the new device resulted in fracture healing in all cases. Generally, revision surgery was unrelated to the new device; the re-fracture seen in two cases was related to further trauma. The assessment of the mobility status of the patients showed that seven of the 18 patients regained the mobility status that they had prior to trauma. Eleven of the 18 patients did not completely recover from the trauma and required more support or walking aids than before injury. However, fractures were caused by simple falls and, in general, patients were still at risk for further falls even after the fractures healed—as observed in two of the 18 patients. In retrospect, the use of walking aids might have been modified so that more suitable aids were used in order to prevent further falls from occurring.

In summary, the new inserts required a higher torsional moment for displacement than the standard plate insert in the biomechanical setup. As a result, the achievable rotational stability seems to be sufficient in the clinical setting with thin cortical bone, where screws and conventional inserts cannot be applied in an adequate manner.

Conclusion

The use of the new plate inserts resulted in a higher rotational fixation strength according to a simplified biomechanical model. The extracortical plate fixation in combination with cerclage wires showed fracture healing in all patients in

difficult to treat fractures by conventional means. Therefore, the new device may be a valuable addition to the existing range of implants especially in cases with bulky revision stems in situ and/or poor bone stock. Based on the presented data, the new plate inserts may be a solution for an increasing number of periprosthetic fractures in the elderly presenting with the reported fracture and implant characteristics.

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Conflict of interest The authors declare that they have no conflict of interest.

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